



4th Asia-Pacific Conference on Plasma Physics, 26-31 Oct, 2020, Remote e-conference

First principle scenario modelling of the Divertor Tokamak Test facility

I.Casiraghi^{1,2}, P.Mantica², F.Koechl³, R.Ambrosino⁴, B.Baiocchi², J.Citrin⁵, L.Frassinetti⁶,
A.Mariani², P.Vincenzi⁷, P.Agostinetti⁷, A.Cardinali⁸, S.Ceccuzzi⁸, L.Figini², G.Granucci²,
T.Johnson⁶, P.Martin⁷, G.Spizzo⁷, M.Valisa⁷, G.Vlad⁸

¹Università degli Studi di Milano-Bicocca, Milano, Italy, ²Istituto per la Scienza e la Tecnologia dei Plasmi, CNR, Milano, Italy, ³CCFE, Culham Science Centre, Abingdon, UK, ⁴Università degli Studi di Napoli Federico II and Consorzio CREATE, Napoli, Italy, ⁵FOM Institute DIFFER, Eindhoven, The Netherlands, ⁶Fusion Plasma Physics, ECSS, KTH Royal Institute of Technology, Stockholm, Sweden, ⁷Consorzio RFX, Padova, Italy, ⁸ENEA, Dipartimento Fusione e Sicurezza Nucleare, Frascati, Italy

e-mail (speaker): i.casiraghi3@campus.unimib.it

The construction of the D-shaped superconducting tokamak DTT (Divertor Tokamak Test facility) [1-3] is starting in Frascati, Italy. The main task of DTT is to study the controlled power and particle exhaust from a fusion reactor, which is a main research topic in the European Fusion Roadmap [4]. Alternative divertor configurations and improved plasma facing materials will be developed and tested in DTT, thanks to its high flexibility in magnetic configurations and divertor choice. A large amount of auxiliary heating (~45MW in the full power scenario) is provided by a 170GHz ECRH system, a 60-90 MHz ICRH system, and a system of 400keV negative ion beam injectors. The precise heating mix has still to be defined. The characteristics of DTT ($R=2.14\text{m}$, $a=0.65\text{m}$, $BT \leq 6\text{T}$, $I_p \leq 5.5\text{MA}$, pulse length $\leq 100\text{s}$) make it ITER and DEMO relevant.

In order to support the DTT design and the planning of its scientific work-program, first-principle based multi-channel integrated modelling of plasma profiles in different operational scenarios is required. The simulation results help to optimise the heating mix and provide scenarios for the design of diagnostics and pellet injectors, for calculations of heat and neutron loads, and for the assessment of issues such as ripple losses.

The DTT simulations have mainly been carried out with the JINTRAC [5] suite with the JETTO [6] transport solver. The simulations predict steady-state radial profiles of electron and ion temperature, density, current density, impurity densities and rotation within the separatrix. The impurity (Ar and W) densities and radiation are simulated with SANCO [7]. The ESCO code calculates a self-consistent equilibrium keeping fixed the boundary provided by the free boundary CREATE-NL solver [8]. In some cases, the ASTRA [9] transport solver has also been used to predict temperatures and density with fixed equilibrium, heating, toroidal rotation and impurities, taken from JINTRAC. The Europed code [10] calculates the pedestal using the EPED1 model [11], providing the boundary conditions for the simulations. The turbulent transport is calculated by the QuaLiKiz [12] or TGLF SAT1 [13] models, while the neoclassical transport is calculated by the Romanelli-Ottaviani model [14] for impurities and NCLASS [15] for main particles. The heating is modelled by GRAY [16] for ECRH, by PENCIL [17] for NBI, and PION [18] for ICRH.

Modelling results of 8 full power H-mode scenarios with Single Null (SN) divertor configuration have been compared to assist the forthcoming heating mix choice. The electron density has a moderately peaked profile and at the plasma center it reaches values in the range of $2.2 \cdot 10^{20} \text{m}^{-3} < n_{e0} < 2.7 \cdot 10^{20} \text{m}^{-3}$. In the central region, the electron temperature T_e is in the range of 17-25keV, while ion temperature T_i is in the range of 8-13keV. This is due to the large and localized ECH power density and the high ion stiffness. The radiated power is around 15MW. In all cases a large amount of thermal power (~15MW) is exchanged from electron to ions. Depending on the sharing between the heating systems, the energy confinement time varies in the range of 0.25-0.5 and the DD neutron rate is in the range of $(0.8-1.7) \cdot 10^{17} \text{s}^{-1}$ (~30% thermal). In addition, scenarios with reduced power for the initial phase of operations have been modelled, and configurations with negative values of triangularity have been explored.

References

- [1] DTT Interim Design Report, ENEA, 2019.
- [2] Special Section of Fusion Engineering and Design, Vol. 122, 2017, 253-294, e1-e25.
- [3] P.Martin et al., Proc. 46th EPS Conference on Plasma Physics, Milano, 2019, ECA Vol. 43C, O2.102.
- [4] A.J.H.Donné, Phil. Trans. R. Soc. A 377 20170432, 2018.
- [5] M.Romanelli et al., Plasma and Fusion Research, 9, 3403023, 2014.
- [6] G. Cenacchi and A. Taroni. Jetto a free boundary plasma transport code. ENEA-RT-TIB, 88-5, 1988.
- [7] L.Lauro Taroni et al., Proc. 21st EPS Conf. on Contr. Fus. and Plasma Phys. (Montpellier, 1994) 1, 102.
- [8] R.Ambrosino, R.Albanese and M.Mattei. Fusion Engineering and Design, 96-97:664 – 667, 2015.
- [9] G.V. Pereverzev et al., Max-Planck Report, IPP 5/98, 2002.
- [10] S. Saarelma et al., Plasma Phys. Control. Fusion 60, 014042, 2018.
- [11] P.B. Snyder et al., Phys. Plasmas 16 056118, 2009.
- [12] J.Citrin et al., Plasma Phys. Control. Fusion 59, 124005, 2017.
- [13] G.M.Staebler et al., Phys. Plasmas 23, 062518, 2016.
- [14] M.Romanelli, M.Ottaviani. Plasma Physics and Controlled Fusion, 40(10):1767–1773, oct 1998.
- [15] W A Houlberg et al. Phys. Plasmas 4, 3230, 1997.
- [16] D. Farina, Fusion Sci. Technol. 52, 154, 2007.
- [17] C.D. Challis et al., Nucl.Fusion 29 563, 1989.
- [18] L.G. Eriksson et al. Nucl.Fusion 33 1037, 1993.